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**Chemical Engineering** 

Technology

# Angular Dependence of $Si_3N_4$ Etching in $C_4F_6/CH_2F_2/O_2/Ar$ Plasmas

The dependence of  $Si_3N_4$  etching on ion-incident angles is investigated at various  $CH_2F_2$  flow rates in  $C_4F_6/CH_2F_2/O_2/Ar$  plasmas. The normalized etch yield (NEY) curves for  $Si_3N_4$  imply that physical sputtering is a major contributor to  $Si_3N_4$  etching. An increase in the amount of  $CH_2F_2$  in the plasma produces thicker and more etch-resistant fluorocarbon films. Systematic analyses on deposition and etching of the passively deposited fluorocarbon films on  $Si_3N_4$  in a  $C_4F_6/CH_2F_2/O_2/Ar$  plasma show that the normalized deposition rate of the fluorocarbon film is nearly the same and unaffected by the  $CH_2F_2$  flow rate while etching of fluorocarbon films is similar to etching of  $Si_3N_4$ , thus, etching of the fluorocarbon film, rather than its deposition, limits  $Si_3N_4$  etching in  $C_4F_6/CH_2F_2/O_2/Ar$  plasmas.

Keywords: Angular dependence, Etch yields, Fluorocarbon films, Physical sputtering,  $Si_3N_4$  etching

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## 1 Introduction

Silicon nitride (Si<sub>3</sub>N<sub>4</sub>) is a dielectric material widely applied in the fabrication of microelectronic devices. It is used primarily as insulation between conducting layers, diffusion and ion implantation masks, and passivation [1]. In recently developed ultralarge-scale integrated (ULSI) circuit technology, the role of Si<sub>3</sub>N<sub>4</sub> films has grown because they serve as etch stop layers for self-aligned contact (SAC) structures and as gate spacers for the formation of doped regions [2-4]. The application of Si<sub>3</sub>N<sub>4</sub> as an etch stop layer and a gate spacer requires good control over the relative etch rate of Si<sub>3</sub>N<sub>4</sub>, i.e., etch selectivity. For example, high silicon oxide (SiO2)-to-Si3N4 etch selectivity is strongly required for SAC etching. However, the Si<sub>3</sub>N<sub>4</sub> etch rate frequently increases at corners and inclined surfaces [3] resulting in low SiO<sub>2</sub>-to-Si<sub>3</sub>N<sub>4</sub> etch selectivity at curved Si<sub>3</sub>N<sub>4</sub> surfaces, leading to failures in SAC etching. Therefore, it is essential to understand the angular dependence of the Si<sub>3</sub>N<sub>4</sub> etch rate in order to predict and control etch selectivities and profiles.

To investigate the angular dependence of the Si<sub>3</sub>N<sub>4</sub> etch rate, it is necessary to precisely control the direction of ions that are incident on the surface of a substrate. Angular dependences of Si<sub>3</sub>N<sub>4</sub> etch rates using ion beam etching [5] and V-groove microstructures [6] were reported. The ion beam apparatus could control the ion-incident angle  $\theta$ , but its low operating pressure depressed the radical concentration too much for plasma etching to be practical. V-groove samples enabled experiments under practical plasma etching conditions, but only a few ionincident angles were available.

Faraday cages have been used extensively to study the angular dependences of etch rates of various surfaces [7–12]. A

Faraday cage is a closed box made from a conductor. If the top plane of the cage is made from conductive grids with diameters smaller than the sheath thickness, ions will enter perpendicular to the sheath formed along it. Since the electric potential in the cage is uniform and unaffected by electric fields outside the cage, the ions travelling inside the cage maintain their initial direction. Therefore, the use of a Faraday cage allows to accurately control the direction of ions incident on the substrate under practical plasma etching conditions by simply varying the angle of the substrate inside the cage.

Lee et al. [12] reported the angular dependences of  $Si_3N_4$ etch rates at various bias voltages in a  $C_4F_8$  plasma using a Faraday cage. They correlated the change in the etch yield with the thickness of a steady-state fluorocarbon film formed on the substrate. They successfully observed the angular dependence of the  $Si_3N_4$  etch rate under practical plasma etching conditions, but the discharge gas,  $C_4F_8$ , was perfluorocarbon (PFC). PFCs are problematic from an environmental viewpoint because they have long atmospheric lifetimes and high global warming potentials [13–15]. Unsaturated fluorocarbons like  $C_4F_6$  have been considered as alternatives to PFCs [16, 17].

In this study, the angular dependences of Si<sub>3</sub>N<sub>4</sub> etch rates in C<sub>4</sub>F<sub>6</sub>/CH<sub>2</sub>F<sub>2</sub>/O<sub>2</sub>/Ar plasmas were investigated using a Faraday cage system. The etching characteristics of Si<sub>3</sub>N<sub>4</sub> were studied by varying the ion-incident angles and CH<sub>2</sub>F<sub>2</sub> flow rates. The

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effects of  $CH_2F_2$  were also examined by analyzing the fluorocarbon films formed on the surface of the substrate during  $Si_3N_4$  etching.

# 2 Experimental

 $\rm Si_3N_4$  etching was performed in an inductively coupled plasma system as displayed in Fig. 1. The diameters of a reaction chamber and an electrode were 200 and 110 mm, respectively. Both the reaction chamber and electrode were made of stainless steel. The plasma was ignited in the reaction chamber by applying a 13.56-MHz radiofrequency (rf) source power to an induction coil. Another 13.56-MHz rf power was used to apply a bias power to the electrode. A quartz window was located below the induction coil, and the distance between the dielectric window and the electrode was 100 mm.

A Faraday cage was used to control the direction of ions that are incident on the sample. The Faraday cage was attached to the electrode. Fig. 2 shows a schematic diagram of the Faraday cage and the arrangement of the samples. The Faraday cage was cylindrical and made from stainless steel. The inner diameter and height of the cage were 80 and 20 mm, respectively. The top plane of the cage was a stainless-steel grid. The grid diameter and pitch were 0.025 and 0.229 mm, respectively. The ionincident angle  $(\theta)$  was defined as the angle between the ionincident direction and the surface normal to the sample. As mentioned earlier, the sheath forms along the top plane of the cage and its interior is free of electric fields. Therefore, the angle of ions incident on a sample can be controlled by varying the angle of the sample holder. In this study, the angle of the sample holder was varied between 0 and 90°. The samples were 470 nm thick Si<sub>3</sub>N<sub>4</sub> films on p-type Si wafers. The Si<sub>3</sub>N<sub>4</sub> films were obtained by low-pressure chemical vapor deposition. The sample was in the form of a  $10 \times 5 \text{ mm}^2$  rectangle. A 1 mm thick quartz bottom plate was placed below the sample holder to mimic the hole structure of microelectronic devices.

A  $C_4F_6/CH_2F_2/O_2/Ar$  plasma was used for  $Si_3N_4$  etching. The total flow rate of the discharge gas was 40 sccm. The flow rates of  $C_4F_6$  and  $O_2$  were fixed at 6 and 1 sccm, respectively.



Figure 1. Schematic diagram of an inductively coupled plasma system equipped with a Faraday cage.



**Figure 2.** Schematic diagrams of a Faraday cage and the substrate arrangement in the cage. The ion-incident angle  $\theta$  was defined as the angle between the ion-incident direction and the surface normal to the substrate.

The flow rate of  $CH_2F_2$  was varied from 0 to 5 sccm. Therefore, the fraction of  $CH_2F_2$  in the input gas, i.e., ratio of the  $CH_2F_2$ flow rate to the total flow rate, ranged from 0 to 12.5%. The flow rate of Ar was then modulated such that the combined flow rate of  $C_4F_6$ ,  $CH_2F_2$ ,  $O_2$ , and Ar was 40 sccm. The pressure in the chamber was 9 mTorr. The source power and bias voltage were 150 W and -450 V, respectively.

The etch rates of the samples were determined by measuring changes in the thickness of the substrate film before and after etching using a thickness meter (model SpecraThick 2000-Deluxe). In all cases, the thickness was measured at 8 mm from the bottom of the sample holder.

The characteristics of a fluorocarbon films formed on the  $Si_3N_4$  surface were analyzed by X-ray photoelectron spectroscopy (XPS). The atomic ratio of fluorine to carbon in the fluorocarbon films was calculated from the C 1s XPS peaks of the film.

## 3 Results

Fig. 3 a shows the change in the etch rate (ER) of  $Si_3N_4$  with the ion-incident angle at various  $CH_2F_2$  flow rates. The etch

rates decrease with increasing CH<sub>2</sub>F<sub>2</sub> flow rate at all ion-incident angles. This results from the reduction in F radicals, which are etchants for Si<sub>3</sub>N<sub>4</sub>, by H atoms coming from CH<sub>2</sub>F<sub>2</sub>. H atoms can react with F radicals to form HF [17]. In the absence of CH<sub>2</sub>F<sub>2</sub>, the etch rate decreases monotonically with ionincident angle. On the other hand, in the presence of CH<sub>2</sub>F<sub>2</sub>, the etch rates increase with ion-incident angle, reach maxima at angles about 40°, and decrease with further increase in the ion-incident angle. This behavior becomes more prominent as the fraction of CH<sub>2</sub>F<sub>2</sub> in the input gas increases. This can be better observed using the nor-



**Figure 3.** Angular dependences of (a) etch rates and (b) normalized etch rates of  $Si_3N_4$  with various  $CH_2F_2$  fractions in the input gas. The  $CH_2F_2$  fraction was based on the total flow rate of the discharge gas.

malized etch rate (NER) curve. The NER is defined as the etch rate at a specific angle normalized to the etch rate on the horizontal surface, i.e.,  $ER(\theta)/ER(0^\circ)$ .

Fig. 3 b illustrates the NER of  $Si_3N_4$  as a function of ion-incident angle with various  $CH_2F_2$  flow rates. In the NER curve, the dotted line indicates a cosine curve representing the change in the flux of ions incident on the sample with their angles. When the  $CH_2F_2$  fraction is increased from 0 to 12.5%, the NERs are higher than the cosine curve at ion-incident angles between 0 to 60°. All of the NERs fall below the cosine curve when the ion-incident angle is higher than 80°. When the ion-incident angle optimized of etching at this angle.

When ion-surface interactions are investigated at various ion-incident angles, it is more relevant to use the etch yield (EY) than the etch rate [7]. The etch yield is defined as the etch rate per ion flux on the substrate surface. Since ion flux is proportional to  $\cos\theta$ , the etch yield excludes the ion flux variations driven by the incident angle.

Fig. 4 displays the normalized etch yield (NEY) of  $Si_3N_4$  as a function of ion-incident angle. The NEY is defined as the etch



Figure 4. Angular dependences of normalized etch yields of Si\_3N\_4 at various CH\_2F\_2 flow rates.

yield at a specific angle divided by the etch yield on the horizontal surface  $[EY(\theta)/EY(0^{\circ})]$ , which is equal to NER( $\theta$ )/cos  $\theta$ . The angular dependence of the NEY exhibit maxima between 50 and 70° at all CH<sub>2</sub>F<sub>2</sub> flow rates. In the absence of CH<sub>2</sub>F<sub>2</sub>, the NEY exhibits maxima at 70°. As the CH<sub>2</sub>F<sub>2</sub> fraction in the input gas is increased to 12.5%, the maximum NEY increases to 3.0 and the angle at which the maximum is reached declines from 70 to 50°.

The shapes of the etch yield curves provide information on the etching mechanism. Possible mechanisms include ionenhanced chemical etching and physical sputtering [18]. When ion-enhanced chemical etching dominates, the etch yield decreases monotonically with the ion-incident angle. On the other hand, when physical sputtering dominates, the etch yield exhibits maxima at angles between 40 and 70°. The NEY curves of Si<sub>3</sub>N<sub>4</sub> in Fig. 4 suggest that physical sputtering is a major contributor to Si<sub>3</sub>N<sub>4</sub> etching in C<sub>4</sub>F<sub>6</sub>/CH<sub>2</sub>F<sub>2</sub>/O<sub>2</sub>/Ar plasmas. However, the maximum NEY value and the ion-incident angle at which this maximum is observed change with the CH<sub>2</sub>F<sub>2</sub> flow rate. This means that the extent to which physical sputtering contributes to Si<sub>3</sub>N<sub>4</sub> etching is dependent on the amount of CH<sub>2</sub>F<sub>2</sub> used.

# 4 Discussion

When a substrate is exposed to fluorocarbon plasmas, e.g.,  $C_4F_6$ , fluorocarbon polymer ( $-C_xF_{y}$ -) films grow on the surface of the substrate. At the same time, the fluorocarbon films are consumed by ion sputtering, F-atom etching, and ion-assisted interactions between the fluorocarbon film and the substrate [4]. At the steady state, a thin fluorocarbon film forms on the substrate surface as a result of competition between fluorocarbon production and consumption. Then,  $Si_3N_4$  substrate etching occurs by forming volatile species such as  $SiF_x$  and  $CNF_y$  via ion bombardment, F-atom interactions, and fluorocarbon film- $Si_3N_4$  interactions. The fluorocarbon film formed on the substrate during etching in fluorocarbon plasmas plays an important role because it acts as an etch barrier against radicals

and ions [7]. As indicated in Fig. 4, the angular dependence of the NEY depended on the  $CH_2F_2$  flow rate. Therefore, the characteristics of the fluorocarbon film must be investigated.

Fig. 5 a displays changes in the deposition rates of passively deposited fluorocarbon films on  $Si_3N_4$  with the ion-incident angle at various  $CH_2F_2$  flow rates. During fluorocarbon film deposition, no bias voltage was applied to the substrate. Except for the bias voltage, the other process conditions were the same as those used in  $Si_3N_4$  etching: 150 W source power, 9 mTorr pressure, 40 sccm total flow rate of  $C_4F_6/CH_2F_2/O_2/Ar$ . The deposition rates of the fluorocarbon films increase with  $CH_2F_2$  flow rate at all ion-incident angles. This is because the addition of  $CH_2F_2$  provides reactive fluorocarbon species such as  $CF_2$ . Since  $CF_2$  radicals are known to be the main precursors for fluorocarbon film formation in fluorocarbon plasmas [16], thicker fluorocarbon films are deposited on the substrate as more  $CH_2F_2$  is introduced.



**Figure 5.** Angular dependences of (a) deposition rates and (b) normalized deposition rates of passively deposited fluorocarbon films on Si<sub>3</sub>N<sub>4</sub> in a C<sub>4</sub>F<sub>6</sub>/CH<sub>2</sub>F<sub>2</sub>/O<sub>2</sub>/Ar plasma at various CH<sub>2</sub>F<sub>2</sub> flow rates.

The deposition rates of the fluorocarbon films decrease monotonically with increasing ion-incident angle at all  $CH_2F_2$  flow rates. In order to clarify the angular dependence of the change in the deposition rate with the  $CH_2F_2$  flow rate, the

normalized deposition rate (NDR) was plotted at various  $CH_2F_2$  flow rates in Fig. 5 b. Similarly to the definition of the normalized etch rate (see Fig. 3 b), the NDR is defined as the deposition rate (DR) at a specific angle normalized to the deposition rate on the horizontal surface, i.e.,  $DR(\theta)/DR(0^\circ)$ . The NDR presented in Fig. 5 b nearly falls on a single curve, regardless of the  $CH_2F_2$  flow rate. This implies that  $Si_3N_4$  etching is not limited by deposition of the fluorocarbon film although its deposition rate increases with the  $CH_2F_2$  flow rate.

Fig. 6 shows fluorine-to-carbon (F/C) ratios of passively deposited fluorocarbon films deposited at various fractions of  $CH_2F_2$ . The F/C ratios were obtained from the carbon 1s X-ray photoemission spectra of the films [4]. For analysis of the F/C ratio, the fluorocarbon films deposited at an ion-incident angle of 0° were used. The F/C ratio of the fluorocarbon film decreases with increasing  $CH_2F_2$  flow rate. As mentioned earlier, H atoms from  $CH_2F_2$  can react with F to form HF. This reduces the number of F radicals in the plasma, and produces a more fluorine-depleted fluorocarbon film. These defluorinated fluorocarbon films have high etch resistance because of an increase in the carbon-to-carbon cross-linking of the film [17].



Figure 6. F/C ratios of passively deposited fluorocarbon films deposited at various  $CH_2F_2$  flow rates. The ion-incident angle was 0°.

This relationship between etch resistance of the fluorocarbon film and CH<sub>2</sub>F<sub>2</sub> flow rate was confirmed by etching the fluorocarbon film. Fig. 7 presents the etch rates and NERs of passively deposited fluorocarbon films on Si<sub>3</sub>N<sub>4</sub> in C<sub>4</sub>F<sub>6</sub>/CH<sub>2</sub>F<sub>2</sub>/O<sub>2</sub>/Ar plasmas as a function of the ion-incident angle at various CH<sub>2</sub>F<sub>2</sub> flow rates. The fluorocarbon films were etched under the same conditions as those for Si<sub>3</sub>N<sub>4</sub> etching. As expected, the etch rate of the fluorocarbon film decreases with increasing CH<sub>2</sub>F<sub>2</sub> flow rate at all ion-incident angles. It is interesting to note that the shapes of the etch rate, or even NER, versus ionincident angle curves from fluorocarbon film etching are very similar to those produced during Si<sub>3</sub>N<sub>4</sub> etching (see Fig. 3). When  $CH_2F_2$  is absent (0%), the etch rate of the fluorocarbon film decreases monotonically with the ion-incident angle. However, when  $CH_2F_2$  is added, the etch rate of the film rises, reaches a maximum at 50°, and declines with increasing ionincident angle.

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Figure 7. Angular dependences of (a) etch rates and (b) normalized etch rates of passively deposited fluorocarbon films on  $Si_3N_4$  in a  $C_4F_6/CH_2F_2/O_2/Ar$  plasma at various  $CH_2F_2$  flow rates.

The similarities between the angular dependences of the etch rates of the fluorocarbon film and  $Si_3N_4$  substrate can be more clearly seen by analyzing the normalized etch yield (NEY). Fig. 8 illustrates the NEYs of the passively deposited fluorocarbon films on  $Si_3N_4$  as a function of the ion-incident angle with various  $CH_2F_2$  flow rates. Much like the NEY curve from  $Si_3N_4$ etching (see Fig. 4), the NEY in this experiment exhibits a maximum at 70° in the absence of  $CH_2F_2$ . Furthermore, as the  $CH_2F_2$  fraction increases to 12.5%, the maximum NEY increases and the angle at which it is reached changes from 70 to 50°.

As indicated in the graph that relates the NDR of the fluorocarbon film and the ion-incident angle at various  $CH_2F_2$  flow rates (Fig. 5 b), the deposition of fluorocarbon films dose not play an important role in determining  $Si_3N_4$  etch characteristics in  $C_4F_6/CH_2F_2/O_2/Ar$  plasmas. On the other hand, there are similarities between etching of fluorocarbon films and  $Si_3N_4$ . Therefore, fluorocarbon film etching, rather than deposition, limits etching of  $Si_3N_4$  in  $C_4F_6/CH_2F_2/O_2/Ar$  plasmas.



Figure 8. Angular dependences of normalized etch yields of passively deposited fluorocarbon films on Si<sub>3</sub>N<sub>4</sub> in a C<sub>4</sub>F<sub>6</sub>/CH<sub>2</sub>F<sub>2</sub>/ $O_2$ /Ar plasma at various CH<sub>2</sub>F<sub>2</sub> flow rates.

# 5 Conclusions

The angular dependence of Si<sub>3</sub>N<sub>4</sub> etching in C<sub>4</sub>F<sub>6</sub>/CH<sub>2</sub>F<sub>2</sub>/O<sub>2</sub>/Ar plasmas was investigated at various CH<sub>2</sub>F<sub>2</sub> flow rates. The etch rates of Si<sub>3</sub>N<sub>4</sub> decreased monotonically with the ion-incident angle in the absence of CH<sub>2</sub>F<sub>2</sub> while they exhibited maxima at angles around 40° in the presence of CH<sub>2</sub>F<sub>2</sub>. The normalized etch yield (NEY) curves of Si<sub>3</sub>N<sub>4</sub> showed maxima at angles between 50 and 70° at all CH<sub>2</sub>F<sub>2</sub> flow rates, indicating that physical sputtering was a major contributor to Si<sub>3</sub>N<sub>4</sub> etching in C<sub>4</sub>F<sub>6</sub>/CH<sub>2</sub>F<sub>2</sub>/O<sub>2</sub>/Ar plasmas. In addition, the maximum NEY and the ion-incident angle at which it was reached were affected by the CH<sub>2</sub>F<sub>2</sub> flow rate.

The deposition rates of the passively deposited fluorocarbon films on the substrate increased with  $CH_2F_2$  flow rate at all ion-incident angles because the addition of  $CH_2F_2$  provided more  $CF_2$ , which is the main precursor for the formation of fluorocarbon films. Although the deposition rate of the fluorocarbon film changed with the  $CH_2F_2$  flow rate, its normalized deposition rate (NDR) fell on a single curve, regardless of the  $CH_2F_2$  flow rate.

The variations in the  $CH_2F_2$  flow rate also affected the etch rate of the passively deposited fluorocarbon film via its F/C ratio. The F/C ratio of the fluorocarbon film decreased and the film became more defluorinated with increasing  $CH_2F_2$  flow rate. This was driven by F reduction by H atoms from  $CH_2F_2$ . Due to an increase in the etch resistance of the defluorinated fluorocarbon film, the etch rate of the fluorocarbon film declined with rising  $CH_2F_2$  flow rate at all ion-incident angles.

There were close similarities between etching of fluorocarbon films and Si<sub>3</sub>N<sub>4</sub>. The NEYs of both materials exhibited maxima at 70°. As the CH<sub>2</sub>F<sub>2</sub> flow rate was increased to 12.5 %, the maximum NEY became higher and the angle at which it was achieved changed to 50°. Thus, fluorocarbon film etching, rather than deposition, is a limiting factor for Si<sub>3</sub>N<sub>4</sub> etching in C<sub>4</sub>F<sub>6</sub>/CH<sub>2</sub>F<sub>2</sub>/O<sub>2</sub>/Ar plasmas.



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## **Abbreviations**

- DR deposition rate
- ER etch rate
- EY etch yield
- NDR normalized deposition rate
- NER normalized etch rate
- NEY normalized etch yield
- PFC perfluorocarbon
- rf radiofrequency
- SAC self-aligned contact
- ULSI ultralarge-scale integrated
- XPS X-ray photoelectron spectroscopy

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